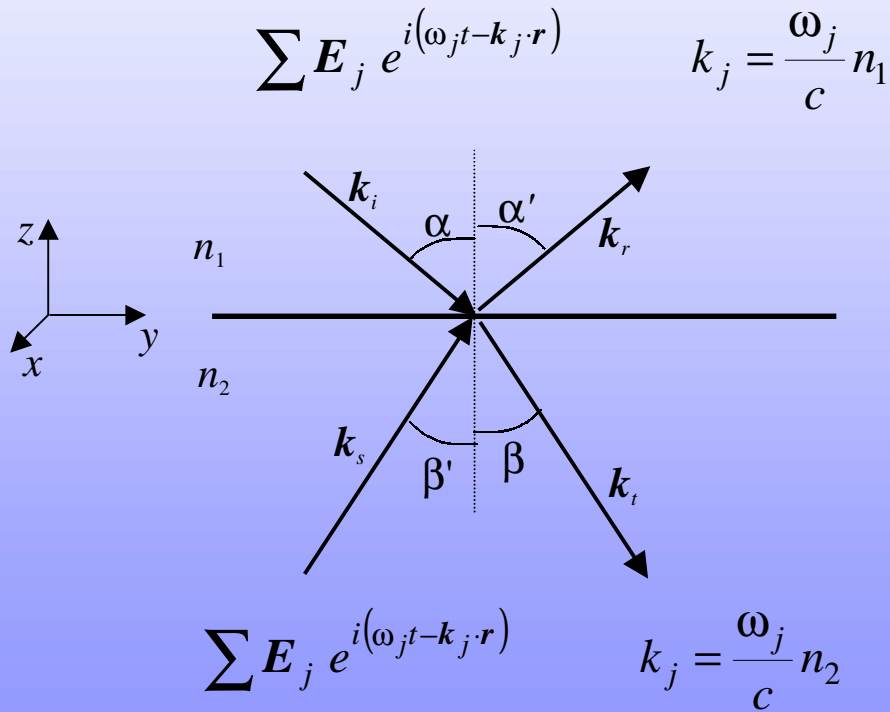


# *Lecture 5: Interfaces between LHI media*

Petr Kužel

- Eigenmodes of electromagnetic field near interfaces: boundary conditions
- Snell's law, Fresnel formulae
- Total reflection, phase shifts
  - ☞ Application: Fresnel prism
- Absorbing media
  - ☞ Application: metal mirrors
- Two parallel interfaces: Fabry-Pérot etalon

# Interface: eigenmodes



Boundary conditions:

For any  $t$ :

$$E_{x1} = E_{x2}$$

$$\omega = \text{const}$$

$$E_{y1} = E_{y2}$$

- For any  $x, y$  in the interface plane:

$$D_{z1} = D_{z2}$$

$$k_x, k_y = \text{const}$$

$$H_{x1} = H_{x2}$$

$$H_{y1} = H_{y2}$$

- Possible  $k_z$ :

$$B_{z1} = B_{z2}$$

$$k_z = \pm \sqrt{\frac{\omega^2}{c^2} n_{1,2}^2 - k_y^2 - k_x^2}$$

# Snell's law

- Choice of the system of axes:

$$k_x = 0$$

- Condition  $k_y = k_i \sin \alpha = \text{const}$ :

$$\alpha = \alpha', \quad n_1 \sin \alpha = n_2 \sin \beta, \quad \beta = \beta'$$

- $z$ -components of the wave vector:

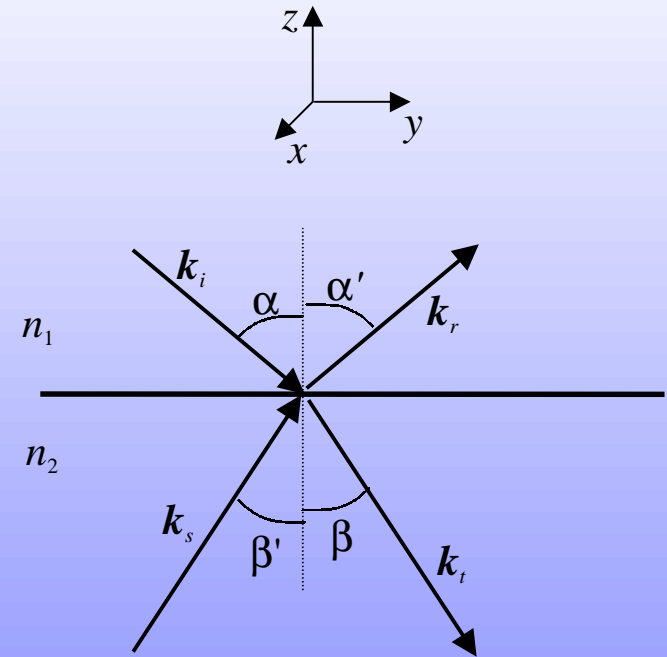
$$k_{z,i} = -\sqrt{n_1^2 \omega^2 / c^2 - k_y^2} = -n_1 \frac{\omega}{c} \cos \alpha$$

$$k_{z,r} = \sqrt{n_1^2 \omega^2 / c^2 - k_y^2} = n_1 \frac{\omega}{c} \cos \alpha$$

$$k_{z,t} = -\sqrt{n_2^2 \omega^2 / c^2 - k_y^2} = -n_2 \frac{\omega}{c} \cos \beta$$

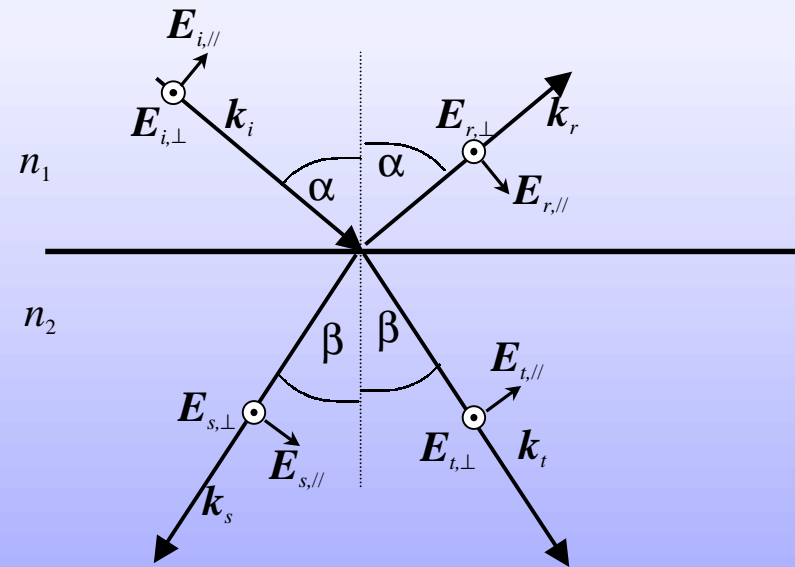
$$k_{z,s} = \sqrt{n_2^2 \omega^2 / c^2 - k_y^2} = n_2 \frac{\omega}{c} \cos \beta$$

- All  $k_z$ -components can be both real and imaginary



# Wave vector and field components

$$\left. \begin{aligned} \mathbf{k}_i &= \frac{\omega n_1}{c} \begin{pmatrix} 0 & s_y^{(1)} & -s_z^{(1)} \end{pmatrix} \\ \mathbf{k}_r &= \frac{\omega n_1}{c} \begin{pmatrix} 0 & s_y^{(1)} & s_z^{(1)} \end{pmatrix} \\ \mathbf{k}_t &= \frac{\omega n_2}{c} \begin{pmatrix} 0 & s_y^{(2)} & -s_z^{(2)} \end{pmatrix} \\ \mathbf{k}_s &= \frac{\omega n_2}{c} \begin{pmatrix} 0 & s_y^{(2)} & s_z^{(2)} \end{pmatrix} \end{aligned} \right\} \begin{aligned} s_y^{(1)} &= \sin \alpha \\ s_z^{(1)} &= \cos \alpha \\ s_y^{(2)} &= \sin \beta \\ s_z^{(2)} &= \cos \beta \end{aligned}$$



$$\mathbf{E}_i = \begin{pmatrix} E_{\perp,i} & E_{\parallel,i} s_z^{(1)} & E_{\parallel,i} s_y^{(1)} \end{pmatrix}$$

$$\mathbf{E}_r = \begin{pmatrix} E_{\perp,r} & -E_{\parallel,r} s_z^{(1)} & E_{\parallel,r} s_y^{(1)} \end{pmatrix}$$

$$\mathbf{E}_t = \begin{pmatrix} E_{\perp,t} & E_{\parallel,t} s_z^{(2)} & E_{\parallel,t} s_y^{(2)} \end{pmatrix}$$

$$\mathbf{E}_s = \begin{pmatrix} E_{\perp,s} & -E_{\parallel,s} s_z^{(2)} & E_{\parallel,s} s_y^{(2)} \end{pmatrix}$$

$$\mathbf{H} = \frac{n}{\eta_0} (\mathbf{s} \wedge \mathbf{E})$$

# Continuity conditions

$$\begin{array}{l}
 E_{x1} = E_{x2} \\
 H_{y1} = H_{y2} \\
 B_{z1} = B_{z2}
 \end{array}
 \qquad
 \begin{array}{l}
 E_{\perp,i} + E_{\perp,r} = E_{\perp,t} + E_{\perp,s} \\
 n_1 s_z^{(1)} (E_{\perp,i} - E_{\perp,r}) = n_2 s_z^{(2)} (E_{\perp,t} - E_{\perp,s}) \\
 n_1 s_y^{(1)} (E_{\perp,i} + E_{\perp,r}) = n_2 s_y^{(2)} (E_{\perp,t} + E_{\perp,s})
 \end{array}
 \qquad
 \begin{array}{l}
 \text{2 independent equations} \\
 \text{2 independent equations}
 \end{array}$$

$$\begin{array}{l}
 E_{y1} = E_{y2} \\
 D_{z1} = D_{z2} \\
 H_{x1} = H_{x2}
 \end{array}
 \qquad
 \begin{array}{l}
 s_z^{(1)} (E_{//,i} - E_{//,r}) = s_z^{(2)} (E_{//,t} - E_{//,s}) \\
 n_1^2 s_y^{(1)} (E_{//,i} + E_{//,r}) = n_2^2 s_y^{(2)} (E_{//,t} + E_{//,s}) \\
 n_1 (E_{//,i} + E_{//,r}) = n_2 (E_{//,t} + E_{//,s})
 \end{array}
 \qquad
 \begin{array}{l}
 \text{2 independent equations} \\
 \text{2 independent equations}
 \end{array}$$

2 independent polarizations: perpendicular ( $\perp$ , TE,  $s$ ) and parallel ( $//$ , TM,  $p$ )

- All wave vectors are real: 4 coupled waves (2 independent + 2 dependent); usual choice:  $E_s = 0$ ,  $E_i =$  incident,  $E_t =$  transmitted,  $E_r =$  reflected.
- Two wave vectors are imaginary: 3 coupled waves (1 independent + 2 dependent);  $E_s$  rejected (divergent),  $E_i =$  incident,  $E_t =$  evanescent,  $E_r =$  totally reflected

# Fresnel equations

$$r_{\perp} = \frac{n_1 \cos \alpha - n_2 \cos \beta}{n_1 \cos \alpha + n_2 \cos \beta}$$

$$t_{\perp} = \frac{2n_1 \cos \alpha}{n_1 \cos \alpha + n_2 \cos \beta}$$

$$r_{//} = \frac{n_1 \cos \beta - n_2 \cos \alpha}{n_1 \cos \beta + n_2 \cos \alpha}$$

$$t_{//} = \frac{2n_1 \cos \alpha}{n_1 \cos \beta + n_2 \cos \alpha}$$

$$r_{\perp} \equiv r_s = -\frac{\sin(\alpha - \beta)}{\sin(\alpha + \beta)}$$

$$t_{\perp} \equiv t_s = \frac{2 \cos \alpha \sin \beta}{\sin(\alpha + \beta)}$$

$$r_{//} \equiv r_p = -\frac{\operatorname{tg}(\alpha - \beta)}{\operatorname{tg}(\alpha + \beta)}$$

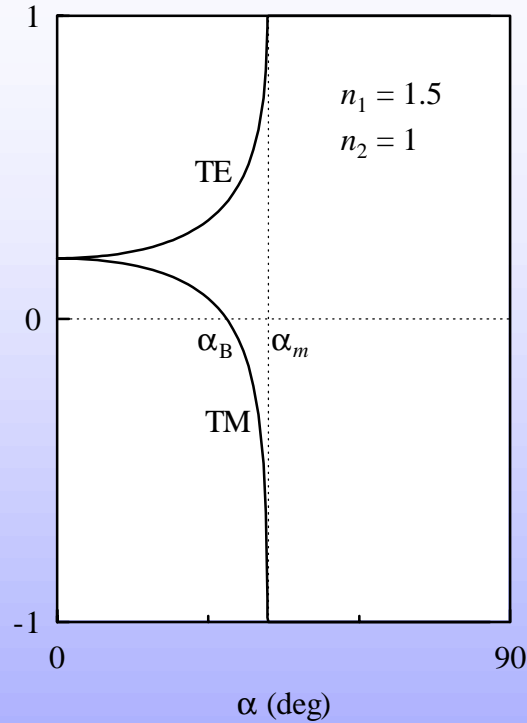
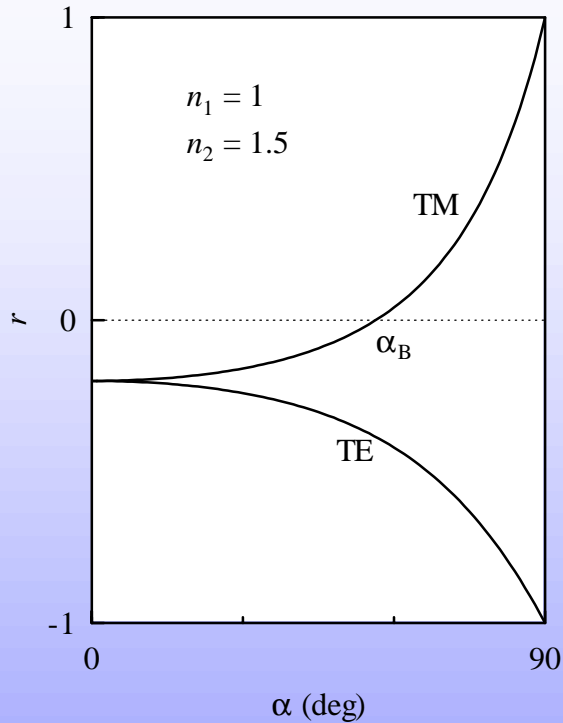
$$t_{//} \equiv t_p = \frac{2 \cos \alpha \sin \beta}{\sin(\alpha + \beta) \cos(\alpha - \beta)}$$

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$$R_{\perp, //} = \frac{S_r \cos \alpha}{S_i \cos \alpha} = \frac{E_r^2}{E_i^2} = r_{\perp, //}^2$$

$$T_{\perp, //} = \frac{S_t \cos \beta}{S_i \cos \alpha} = \frac{n_2 \cos \beta E_t^2}{n_1 \cos \alpha E_i^2} = \frac{n_2 \cos \beta}{n_1 \cos \alpha} t_{\perp, //}^2$$

# Reflected waves



Critical angle  $\alpha_m$  :

$$\sin \alpha_m = n_2/n_1$$

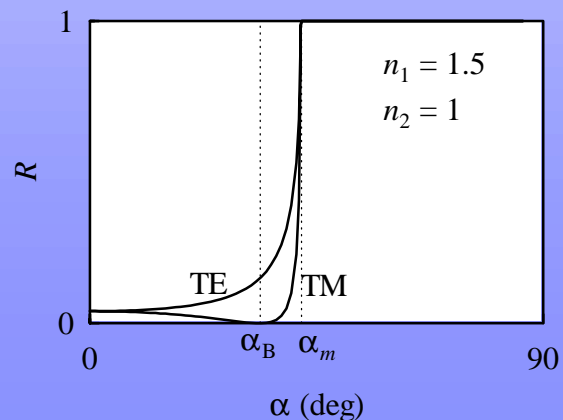
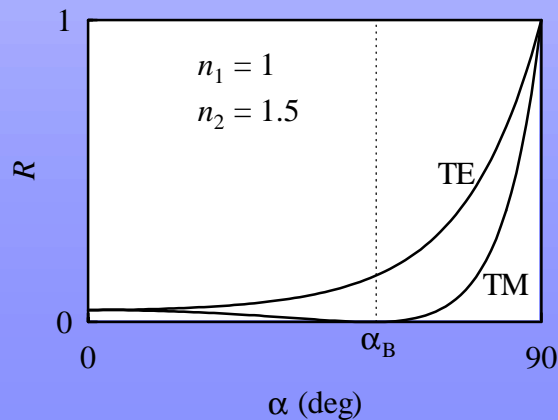
for  $\alpha > \alpha_m$  the wave is totally reflected

Brewster angle  $\alpha_B$  :

$$\text{tg} \alpha_B = n_2/n_1$$

$$\alpha_B + \beta_B = \pi/2$$

$$r_{//} = 0$$



Problem of the phase shifts after reflection:

if  $\mathbf{E}$  is out of phase (shifted by  $\pi$ ) then  $\mathbf{B}$  is in phase and vice versa.

# Total reflection

$$k_{z,t} \left( = -n_2 \frac{\omega}{c} \cos \beta \right) = -\sqrt{\frac{\omega^2}{c^2} n_2^2 - k_y^2} = -n_1 \frac{\omega}{c} \sqrt{n^2 - \sin^2 \alpha} = i n_1 \frac{\omega}{c} \sqrt{\sin^2 \alpha - n^2}$$

with  $n = n_2/n_1 < 1$

$$\mathbf{E}_t = \mathbf{E}_{0t} e^{i(\omega t - \mathbf{k}_t \cdot \mathbf{r})} = \mathbf{E}_{0t} e^{i(\omega t - \mathbf{k}_{t,y} y)} e^{-i k_{t,z} z} = \mathbf{E}_{0t} e^{i(\omega t - \mathbf{k}_{t,y} y)} e^{\frac{z}{2h}} \quad \langle S \rangle \propto e^{-\frac{|z|}{h}}$$

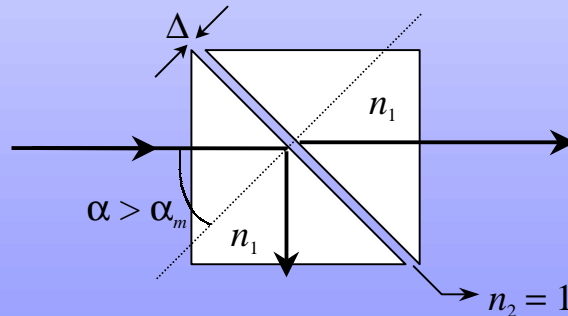


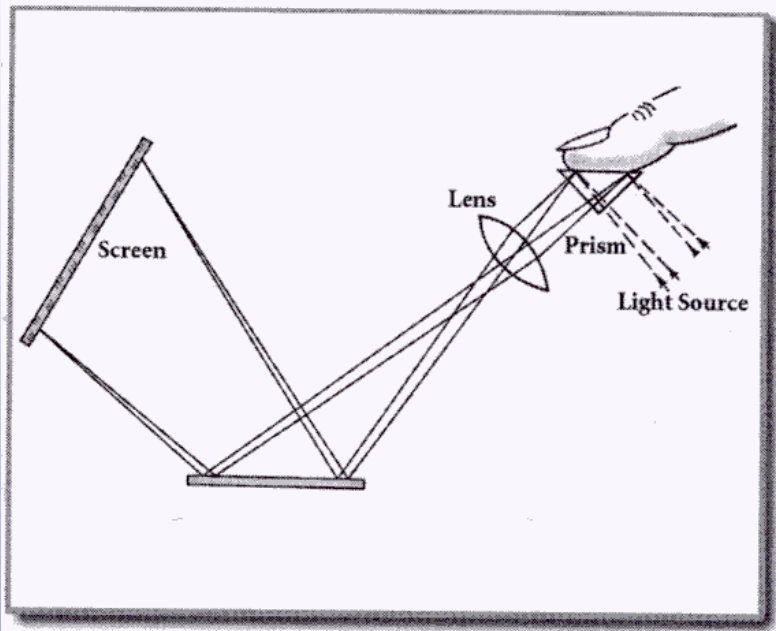
Illustration...

$$\cos \beta = -i \frac{\sqrt{\sin^2 \alpha - n^2}}{n}$$

$\cos \beta$  is then replaced in Fresnel formulae by this new definition



# Total internal reflection: illustration



# Total reflection: continued

$$r_{\perp} = \frac{n_1 \cos \alpha - n_2 \cos \beta}{n_1 \cos \alpha + n_2 \cos \beta} \rightarrow \frac{\cos \alpha + i\sqrt{\sin^2 \alpha - n^2}}{\cos \alpha - i\sqrt{\sin^2 \alpha - n^2}}$$

$$r_{//} = \frac{n_1 \cos \beta - n_2 \cos \alpha}{n_1 \cos \beta + n_2 \cos \alpha} \rightarrow -\frac{n^2 \cos \alpha + i\sqrt{\sin^2 \alpha - n^2}}{n^2 \cos \alpha - i\sqrt{\sin^2 \alpha - n^2}}$$

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$$r_j = \pm \frac{|r_j| e^{i\delta_j/2}}{|r_j| e^{-i\delta_j/2}} = \pm e^{i\delta_j}$$

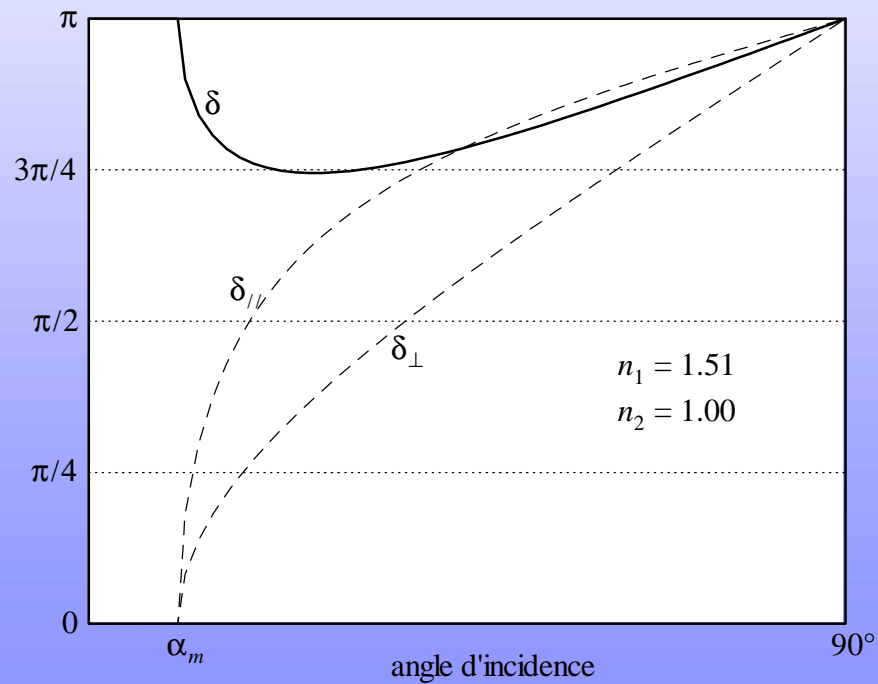
Dephasing between  $\perp$  and  $//$  components:  $\delta = \delta_{\perp} - \delta_{//} + \pi$

$$\operatorname{tg}\left(\frac{\delta_{\perp}}{2}\right) = \frac{\sqrt{\sin^2 \alpha - n^2}}{\cos \alpha}$$

$$\operatorname{tg}\left(\frac{\delta_{//}}{2}\right) = \frac{\sqrt{\sin^2 \alpha - n^2}}{n^2 \cos \alpha}$$

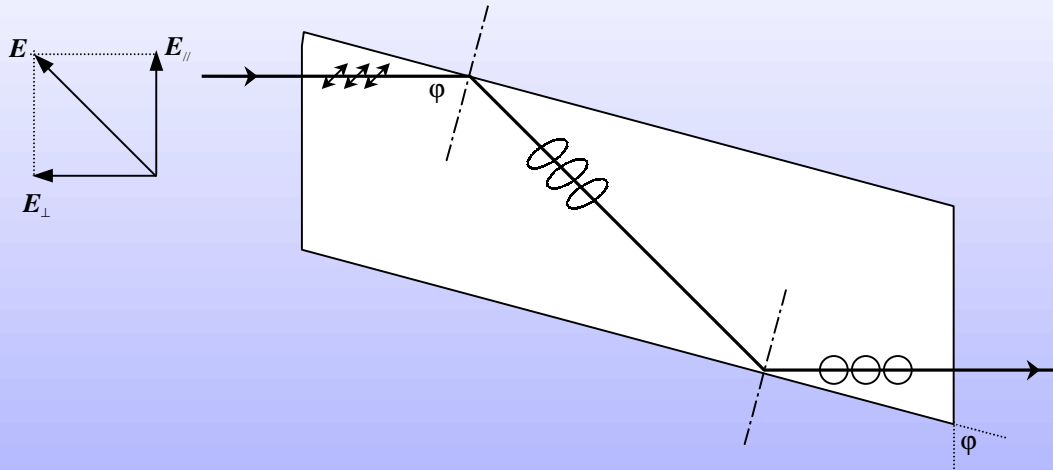
# Total reflection: dephasing

$$\operatorname{tg}\left(\frac{\delta}{2} - \frac{\pi}{2}\right) = \operatorname{tg}\left(\frac{\delta_{\perp}}{2} - \frac{\delta_{\parallel}}{2}\right) = -\frac{\cos \alpha \sqrt{\sin^2 \alpha - n^2}}{\sin^2 \alpha}$$

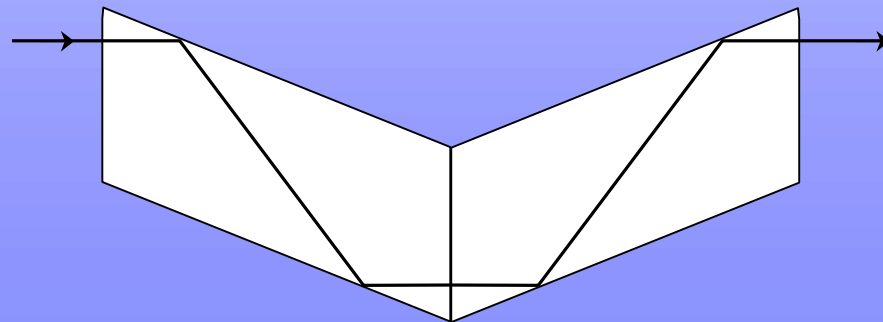


# Total reflection: application

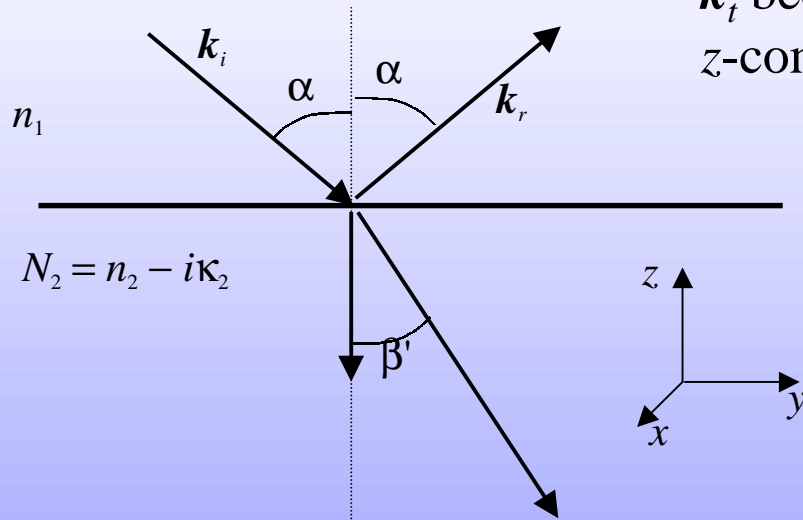
Fresnel prism: quasi-wavelength independent quarter-wave plate



Combination of 2 Fresnel prisms: half-wave plate



# Reflection on an absorbing medium



$k_t$  becomes complex (or strictly speaking its  $z$ -component becomes complex):

$$k_t = k'_t - ik''_t$$

$$k_t = \frac{\omega}{c} \left( 0, \quad n_1 \sin \alpha, \quad -\sqrt{N_2^2 - n_1^2 \sin^2 \alpha} \right)$$

We can formally introduce a complex angle  $\beta$ :

$$N_2 \cos \beta = \sqrt{N_2^2 - n_1^2 \sin^2 \alpha}$$

$$N_2 \sin \beta = n_1 \sin \alpha$$

and use the previously derived Fresnel formulae

# Reflection on an absorbing medium: continued

Two differences with non-absorbing medium should be pointed out:

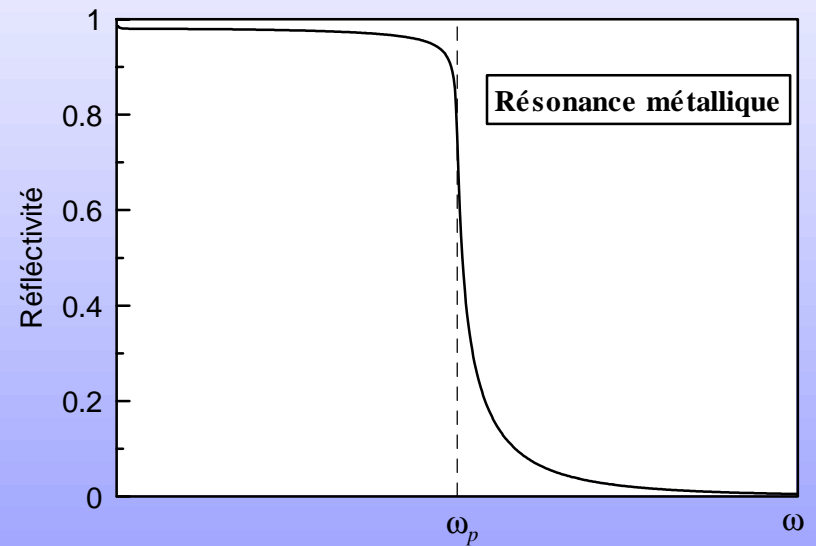
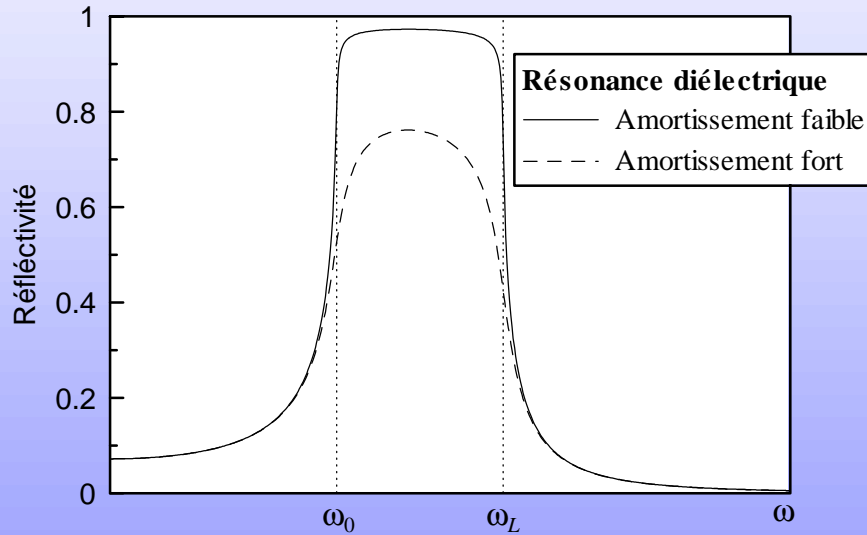
- There is a phase shift due to the absorption:  $r_{\perp}$  and  $r_{//}$  are complex for any angle of incidence
- The absorption increases the reflectivity. One gets for the normal incidence:

$$R = \left| \frac{N-1}{N+1} \right|^2 = \left( \frac{n-i\kappa-1}{n-i\kappa+1} \right) \left( \frac{n+i\kappa-1}{n+i\kappa+1} \right) = \frac{(n-1)^2 + \kappa^2}{(n+1)^2 + \kappa^2} > \frac{(n-1)^2}{(n+1)^2}$$

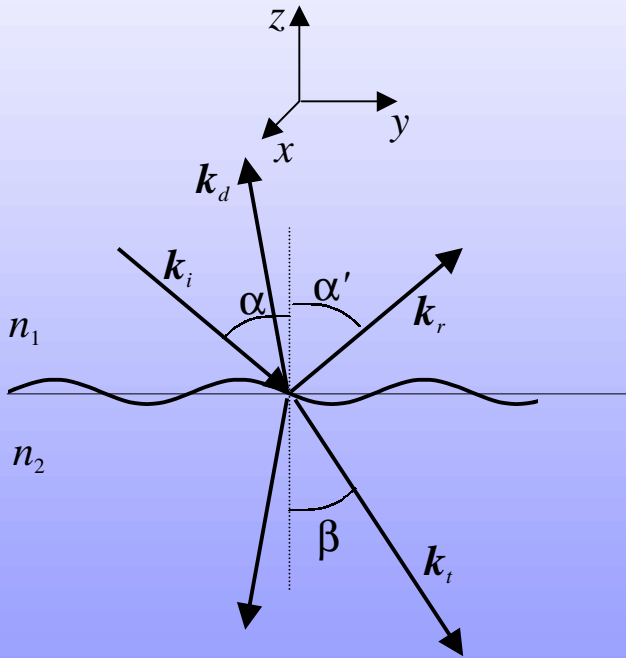
The reflectivity is very large ( $R \rightarrow 1$ ) when:

- The absorption index is large ( $\kappa \gg 1$ ): strongly absorbing medium does not absorb much — it reflects.
- The refractive index vanishes ( $n \rightarrow 0$ ): this happens below the plasma frequency in metals and between the transverse and longitudinal resonance in dielectrics.

# Reflectivity near resonances



# Ondulating surface: second order effects



$$u(y, t) = u_0 e^{i(\Omega t - Q y)}$$

- Interface conditions: continuity at  $z = u$
- First order development:

$$\begin{aligned} E(z = u) &= E_0 e^{i(\omega t - k_y y - k_z u)} \approx E_0 (1 - i k_z u) e^{i(\omega t - k_y y)} = \\ &= E_0 (1 - i k_z u_0 e^{i(\Omega t - Q y)}) e^{i(\omega t - k_y y)} \end{aligned}$$

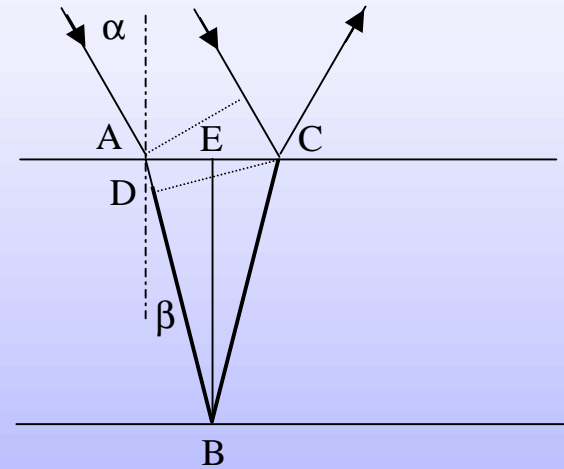
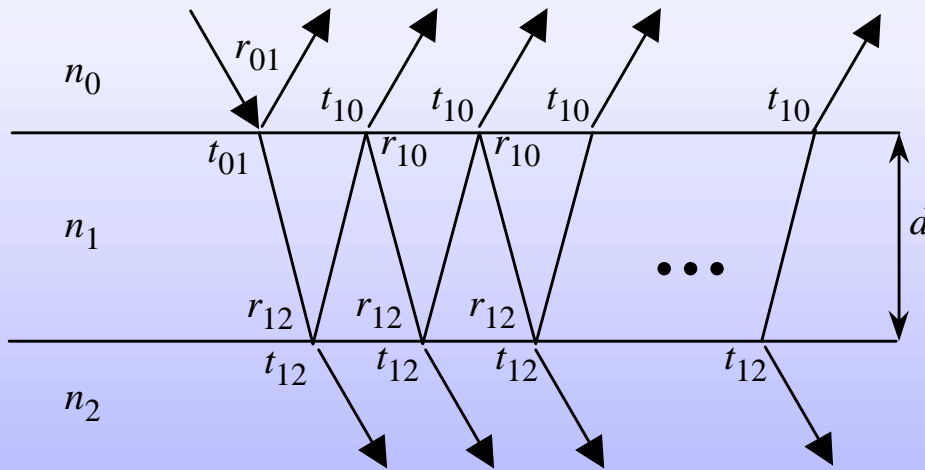
- Waves with new wave vectors and frequencies appear:

$$k_{d,y} = k_y + Q$$

$$\omega_d = \omega + \Omega$$



# Two interfaces: intuitive method



**Difference of the beam paths:**

$$\Delta L n_1$$

$$\Delta L = ABC - AD$$

$$ABC = 2d / \cos\beta$$

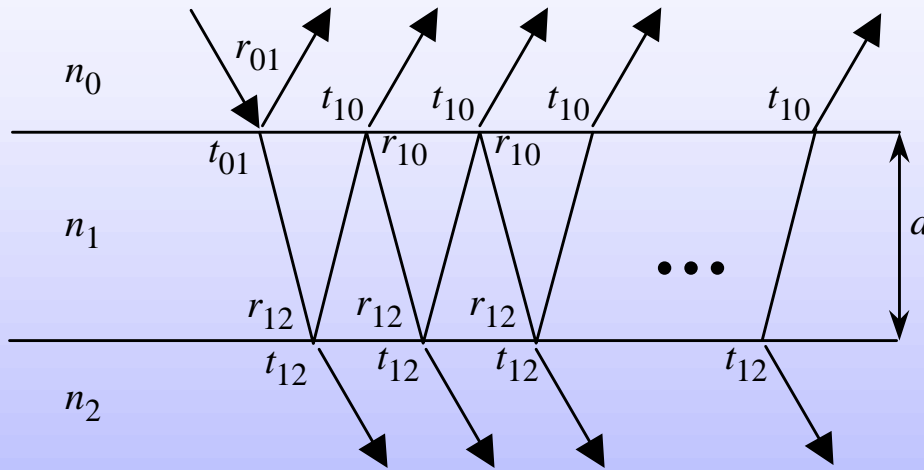
$$AD = AC \sin\beta = 2 AE \sin\beta =$$

$$= 2d \sin\beta \operatorname{tg}\beta$$

$$\Delta L n_1 = 2dn_1 \cos\beta$$

Phase change:  $e^- = e^{-2i\omega nd \cos\beta/c}$

# Sum of partial waves



$$\begin{aligned}
 r &= r_{01} + t_{01}t_{10}r_{12}e^{-} + t_{01}t_{10}r_{12}e^{-}r_{10}r_{12}e^{-} + t_{01}t_{10}r_{12}e^{-}(r_{10}r_{12}e^{-})^2 \dots = \\
 &= -r_{10} + t_{01}t_{10}r_{12}e^{-} \sum_{k=0}^{\infty} (e^{-}r_{10}r_{12})^k = \frac{r_{12}e^{-2i\omega n_1 d \cos \beta / c} - r_{10}}{1 - r_{10}r_{12}e^{-2i\omega n_1 d \cos \beta / c}}
 \end{aligned}$$

$$\begin{aligned}
 t &= t_{01}t_{12} + t_{01}t_{12}r_{12}r_{10}e^{-} + t_{01}t_{12}(r_{12}r_{10}e^{-})^2 + t_{01}t_{12}(r_{12}r_{10}e^{-})^3 + \dots = \\
 &= t_{01}t_{12} \sum_{k=0}^{\infty} (e^{-}r_{10}r_{12})^k = \frac{t_{01}t_{12}}{1 - r_{10}r_{12}e^{-2i\omega n_1 d \cos \beta / c}}
 \end{aligned}$$

# Fabry-Pérot etalon

Plane-parallel plate in the air

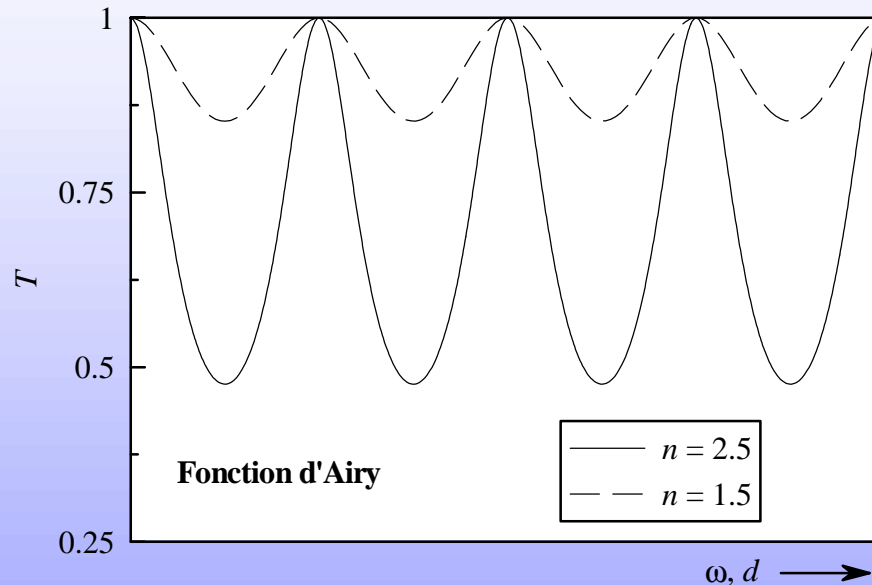
$$\begin{aligned} t &= t_{01}t_{12} + t_{01}t_{12}r_{12}r_{10}e^{-} + t_{01}t_{12}(r_{12}r_{10}e^{-})^2 + t_{01}t_{12}(r_{12}r_{10}e^{-})^3 + \dots = \\ &= t_{01}t_{12} \sum_{k=0}^{\infty} (e^{-}r_{10}r_{12})^k = \frac{t_{01}t_{12}}{1 - r_{10}r_{12}e^{-2i\omega n_1 d \cos \beta / c}} \end{aligned}$$

- Coefficients  $T = tt^*$  et  $R = rr^*$  are calculated
- $n_0 = n_2 = 1$
- $r_{10} = r_{12}$ ,  $R_{10} = r_{10}$ ,  $t_{10} = t_{01}$ ,  $T_{01} = t_{01}$ ,  $T_{10} = t_{10}$

Airy function:

$$T = \frac{T_{01}T_{10}}{(1 - R_{10})^2 + 4R_{10} \sin^2 \varphi} = \frac{1}{1 + \frac{4R_{10}}{(1 - R_{10})^2} \sin^2 \varphi} \quad (\varphi = \omega n_1 d \cos \beta / c)$$

# Airy function



$$T = \frac{1}{1 + \frac{4R_{10}}{(1 - R_{10})^2} \sin^2 \varphi}$$

Maximum ( $T_{max} = 1$ ):

$$\varphi = m \pi$$

$$2n_1 d \cos \beta = m \lambda$$

$$\Delta l + \lambda/2 = (2m + 1) \lambda/2$$

Minimum:

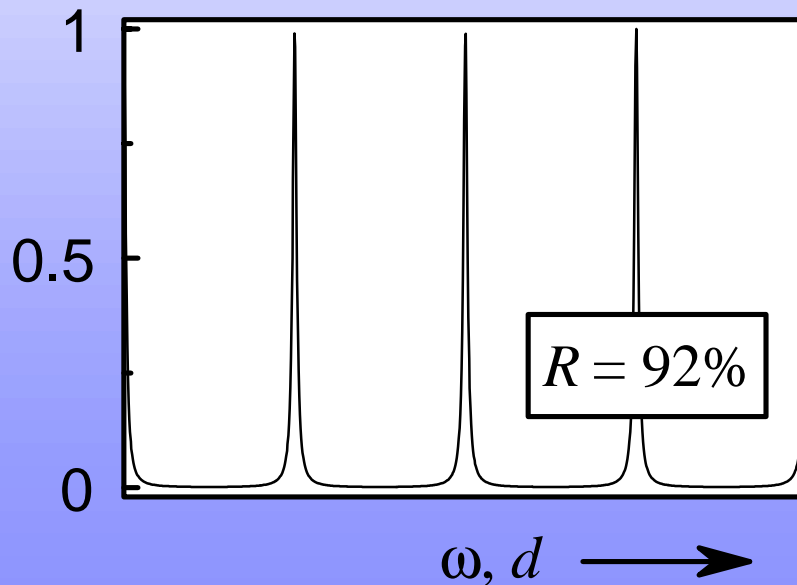
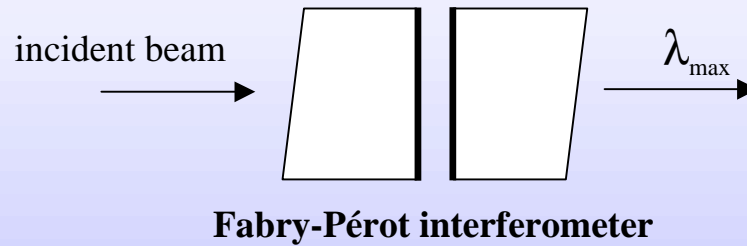
$$\varphi = (2m - 1) \pi/2$$

$$2n_1 d \cos \beta = (2m - 1) \lambda/2$$

$$\Delta l + \lambda/2 = m \lambda$$

$$T_{min} = \left( \frac{1 - R_{10}}{1 + R_{10}} \right)^2$$

# Fabry-Pérot interferometer



$$\lambda_{\max} = \frac{2nd}{m}$$

$$\text{Contrast: } \frac{T_{\max}}{T_{\min}} = \left( \frac{1 + R_{10}}{1 - R_{10}} \right)^2 \approx 550$$

Finesse: 37